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Conductive Elements

Technical Field

The present invention relates to a method of making conductive elements and in particular, to making patterned conductive elements suitable for use in the manufacture of implantable medical devices.

Background

Medical devices that are implanted in the body are subject to a large range of design and manufacturing constraints.

Such medical devices need to be as small as possible to ensure they are minimally invasive. The order of size for components can be in the micron scale.

Further, the materials from which the devices are made must be "biocompatible". This means they must have been proven to not to cause any significant adverse reactions in the body as a result of contact with bodily fluids or tissue, such as tissue death, tumor formation, allergic reaction, foreign body reaction (rejection), inflammatory reaction, or blood clotting. Moreover, biocompatibility means the material must not be susceptible to damage from long-term placement in the body.

The material of choice for conductive elements in implantable medical devices is platinum, following extensive trials performed over the years.

Given the above requirements, the manufacturing of wiring and connector components for implantable medical devices has developed into a labour intensive and highly specialised craft.

One particular area where this is evident is in the field of cochlear implants, which have been developed to provide the sensation of hearing to hearing impaired individuals.

A cochlear implant system bypass the hair cells in the cochlea to directly deliver electrical stimulation to the auditory nerve fibres, thereby allowing the brain to perceive a hearing sensation resembling the natural hearing sensation normally delivered to the auditory nerve. US Patent No. 4,532,930, the contents of which are incorporated herein by reference, describes one type of cochlear implant system.

The intracochlear electrode array has generally been manufactured by positioning a plurality of electrically conductive platinum rings (for example, 22) in a linear array, manually welding electrical conductive wires to each of the electrodes, and then moulding a resiliently flexible carrier member about the array. Each of the wires is insulated from one another to minimise unwanted interaction between different electrical components.

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In view of the high labour cost and complexity associated with the manufacturing of the conductive elements, a number of manufacturing alternatives have been investigated

For example, thin film technology can be used to create electrically conductive features on insulating surfaces on a micron scale. Such techniques include electroforming, vacuum deposition (sputtering, evaporation), and chemical vapour deposition.

However, the metallic films produced by these techniques can feature properties that are different from the corresponding properties of the original, bulk materials used. This results in the materials functioning differently from their intended purpose. Further, the integrity of the biocompatible material must be maintained, by avoiding or reducing any contamination introduced during the manufacturing process.

In the case of platinum, thin film techniques tend to result in cracking and delamination of the platinum. This forms a high impedance path which impairs the functionality of the device.

It is desirable to provide an improved method of manufacturing biocompatible conductive devices in the micron scale.

Summary

According to one aspect of the present invention, there is provided a method of forming a patterned conductive element for an implantable medical device, the method comprising the steps of:

- (i) depositing a supplementary material on a sheet of conductive, parent material to form a sheet of composite material;
- (ii) applying a carrier material over the supplementary material of the composite sheet to form a sheet of semi-finished material;
- (iii) removing portions from at least the conductive parent material of the sheet of semi-finished material in accordance with a desired pattern corresponding to a patterned conductive element to be formed; and
- (iv) releasing at least the carrier material from the sheet of semi-finished material.

According to another aspect of the present invention, there is provided a method of making a sheet of semifinished material, said method comprising the steps of:

depositing a supplementary material on a platinum sheet to form a composite sheet; and

applying a carrier material over the supplementary material, to form a sheet of semi-finished material;

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wherein the platinum sheet on the semi-finished material has a thickness of not more than 100 μ m.

According to another aspect of the present invention, there is provided a method of forming an electrode array for an implantable medical device, said method comprising the steps of:

(i) preparing a semi-finished sheet by depositing a supplementary material on a platinum sheet and then applying a carrier material over the supplementary material;

(ii) removing portions from at least the platinum sheet in accordance with a predetermined pattern, the pattern including a linear array of stimulating or recording pads and at least one electrical conduction means extending away from each one of the pads to a location distal from the pad; and

(iii) releasing the carrier material.

Brief Description of the Drawings

Various exemplary arrangements of the present disclosure will now be described with reference to the drawings, in which:

Fig. 1A is a schematic representation of the steps required to manufacture a semi-finished sheet material used to form an electrode array for an implantable medical device in accordance with one example of this disclosure;

Fig. 1B is a schematic representation of the steps required to manufacture a conductive element for an implantable medical device, starting with the semi-finished sheet material produced by the method of Fig. 1A;

Fig 2A is a plan view of an electrode tip configuration of an electric discharging machine;

Fig 2B is a plan view of the semi-finished sheet material showing a line vapourised by use of the tool of Fig. 2A;

Fig. 2C is a plan view of the semi-finished sheet material of Fig. 2B showing how an electrode and adjoining wire can be formed following a second use of the tool of Fig. 2A;

Fig. 2D is a plan view of the semi-finished sheet material of Fig. 2B depicting how an array of electrodes and adjoining wires are formed by a plurality of uses of the tool of Fig. 2A;

Fig. 3A is a plan view of another electrode tip of an electric discharging machine;

Fig. 3B is a plan view of a semi-finished sheet material showing three lines having been vaporised through use of the tool depicted in Fig. 3A;

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Fig. 3C is a plan view of the semi-finished sheet material of Fig. 3C depicting how three electrodes and adjoining wires can be formed following a second use of the tool of Fig. 3A;

Fig. 3D is a plan view of the semi-finished sheet material of Fig. 3B depicting how an array of electrodes and adjoining wires are formed by a plurality of uses of the tool of Fig. 3A;

Fig. 4 is a plan view of semi-finished sheet material depicting how different sets of electrodes and adjoining wires can be formed in a platinum sheet through appropriate machining;

Fig. 5 is a drawing depicting how sets of electrodes formed using an embodiment of the method defined herein can be stacked on top of each other to form an electrode array suitable for use in a cochlear implant system;

Fig. 6 illustrates a carrier member having an array of curved electrodes with a stylet positioned therein, the carrier being depicted in a configuration ready for insertion into the cochlea of an implantee;

Fig. 7 shows the carrier member of Fig. 6 with the stylet retracted thereby allowing the carrier member to adopt a more pronounced curvature; and

Fig. 8 shows the carrier member of Fig. 6 with the stylet fully retracted thereby allowing the carrier member to adopt its fully curved configuration.

Detailed Description Including Best Mode

An example of a process used to make a semi-finished sheet material that can later be used to form an electrode array will now be described with reference to Fig. 1A.

Commencing with Step 11, a sheet of conductive, biocompatible parent material 1 is sourced. This parent material is most usually platinum, although other materials which have been shown to possess the same properties as platinum for the purposes of suitability as a conductive element in an implantable medical device could also be used. Preferably, the platinum sheet is at least 99.95% pure and has a thickness of approximately 20µm to 40µm, although dimensions in the range of 10µm to 200µm are also envisaged.

Next at Step 12, a supplementary material 2 is deposited on to one side of the platinum sheet 1 to form a new composite sheet 3. In this example, the supplementary material 2 is Titanium Nitride (TiN) and is deposited at a thickness of around 2µm to 4µm on the upper surface. Other materials such as Tantalum (Ta), Niobium (Nb), Nickel (Ni), or Iridium (Ir) could also be used.

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Preferably, the deposition technique uses the "Magnetron" method, which minimises high temperatures thought to be a contributing factor to possible contamination.

Alternatively, the deposition technique can be performed using vacuum cathodic arc deposition and more preferably, using a filtered arc deposition system (FADS) that is described for example in US Patent No. 5,433,836.

FADS uses a macroparticle filter which removes microdroplets of cathode material emitted from the surface of the arcing cathode, which results in a film which is free of microdroplets that are present in films prepared by conventional arc evaporation methods.

Vacuum deposition is the deposition of a film or coating in a vacuum (or low-pressure plasma) environment. Generally, the term is applied to processes that deposit atoms or molecules one at a time, such as in physical vapor deposition (PVD) or low-pressure chemical vapor deposition (LPCVD) processes. It can also be applied to other deposition processes such as low-pressure plasma spraying (LPPS).

After deposition of the supplementary material 2, Step 13 is executed by sourcing and then applying a carrier material to the composite sheet 3, so that the supplementary material 2 is disposed between the parent material 1 and the carrier material 2.

In a first example, the carrier material 2 is a copper sheet and is applied to the composite sheet 3 by co-rolling. This process is known as "roll cladding" and effectively "cold welds" or "crush bonds" the materials together, while reducing the overall thickness of the rolled materials.

Alternatively, the carrier material 4 according to this example can be electroplated to the composite sheet.

Finally, at Step 14, the semi-finished sheet material 5 is produced having the following characteristics:

	Material	Thickness
Parent material	Platinum	20µm to 40µm
Supplementary material	Titanium Nitride	0.5µm to 4µm
Carrier material	Copper	100µm

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Referring now to Fig. 1B, an example of a process used to work the sheet of semi-finished material into a patterned conductive element for an implantable medical device will be described. The patterned conductive element has a plurality of conductive paths and in this example, is formed into an electrode array for a cochlear implant. Whilst the

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example described below uses a micro-machining technique to work the semi-finished material, it is emphasised that the scope of this disclosure includes other methods such as dry etching, where this can be adapted to work for the required micron-scale. Similarly, other micro-machining techniques can be used, such as milling or cutting.

5 Commencing with Step 15, a portion of the sheet of semi-finished material produced by the process of Fig. 1A is cut to a workable size and placed on a work surface of a machine that can perform micromachining, such as electrical discharge machining (EDM). An example of a workable size for the semi-finished material could be approximately 50mm x 250mm, although this will depend on the actual machine and other routine
10 manufacturing variations.

EDM removes material from an electrically conductive work piece by applying a series of electrical discharges between the electrode and the sheet in a dielectric fluid. The electrode melts and vaporises the work piece material but never actually touches the work.

The size and shape of the tip of the electrode, together with the way in which the
15 electrode is moved around and brought to bear on the surface of the conductive work piece, determines the size and shape of the portions that are to be removed.

At Step 16, the EDM is operated by bringing an electrode tip 21 adjacent the semi-finished sheet material. An example of the configuration of the electrode tip 21 is shown in Fig. 2A.

20 The EDM process penetrates the platinum parent material, the TiN supplementary material and at least part of the copper carrier material. The copper carrier material is partly retained during the EDM process to enable easier, subsequent handling of the fragile platinum material.

In the example of Fig. 2A, the EDM equipment relies on use of a single tip 21 that is
25 brought adjacent the sheet 22 at a number of different locations so as to remove differing portions 23 of the sheet 22. As can be seen in Fig. 2D, multiple use of the single tip electrode 21 at different locations on the sheet 22 gradually leads to the creation of a linear array of discrete, substantially rectangular electrodes 25 or stimulating pads. Each electrode has a conducting portion or wire 24 extending away to a location distal the
30 electrode 25.

Typically, each electrode 25 formed in the sheet 22 has a size of about 0.4 mm^2 to 0.5 mm^2 and the width of each respective wire is around $100 \mu\text{m}$ or less, with a similar spacing between neighbouring wires.

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As shown in Fig. 4, the linear wires 24 are aligned in a parallel arrangement for at least a portion of their lengths.

Fig. 3A depicts an alternative electrode tip arrangement, in which three separate electrode tips 21 are arranged to simultaneously remove three regions 23 of sheet 22 as depicted, for example in Fig. 3B.

As depicted in Figs. 3C and 3D, through multiple uses of the EDM, an array of electrodes 25 and associated wires 26 are formed in the sheet 22. The advantage of the use of the arrangement depicted in Fig. 3A is that fewer uses of the EDM tip results in the formation of the same array 24.

Having completed the 'working' or micro-machining of the semi-finished material, Step 17, is then proceeded to. Here, a top side of the worked platinum sheet is cleaned and degreased in preparation for the remaining process steps.

At Step 18, a holding layer is applied to the top side of the worked platinum sheet to increase strength. The holding layer is typically resiliently flexible and also relatively electrically insulating. An example material would be parylene which is typically applied using vapor phase deposition. Alternatively, silicone could be sprayed on to the sheet.

If desired, the electrodes 25 can be masked before the holding layer is applied. Alternatively, the holding layer can be later removed from the electrodes 25, such as by laser ablation, to expose the electrodes.

At Step 19, the layer of copper carrier material is released by way of a chemical etch, for example, by using ammonium persulfate. Where the carrier is copper, this can be achieved by dissolving the copper in a bath. This technique operates on the principle that the copper layer is oxidised and hence dissolved at a potential that is lower than the potential required to oxidise the remaining platinum of the sheet.

Other techniques to remove the carrier material are envisaged, depending on the material used.

Step 20 involves formation of the electrode array, in which the sets of electrodes are stacked one upon the other. The actual position of the electrodes in each set are not necessarily vertically aligned. Rather, the set immediately above its lower set may be laterally offset so as to ensure the electrodes are visible from beneath the stack. An example of a part of a longitudinal array of electrodes 25 is depicted as Fig. 5.

As depicted in Fig. 4, the wires 24 extending from each electrode 25 are of the same length. It can, however, be envisaged that the wires 24 could be formed with different lengths to account for the ultimate offset present when forming the stack.

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Once the stack is formed, the electrodes are deformed so as to at least partially extend in a third dimension. Preferably, each of the electrodes are curved out of the plane of the wires 24 for each set of electrodes. The curvature can be substantially semi-circular. A mandrel can be used to form the curvature in the electrodes.

5 Once the electrodes 25 have been deformed to have a substantially semi-circular curvature, each of the electrodes 25 are further folded about a longitudinal axis of the array 21. This folding of the electrodes 25 serves to bend the electrodes around the wires 24 of the array. The electrodes are folded together and define a lumen that extends through the array 21. An example of the curvature of individual electrodes is depicted in
10 Fig. 6.

Once the electrode array 21 is complete it is encapsulated in a further layer of a biocompatible silicone material to form a electrode carrier member 61. Silastic MDX 4-4210 is an example of one suitable silicone for use in the formation of the carrier member 61. The carrier member can be formed by mounting the array 21 in a mould and filling
15 the mould with silicone and allowing it to cure. In this arrangement, the electrodes are positioned in the mould so as to not be coated with the silicone. In the arrangement depicted in Figs. 6-8, the carrier member is moulded in a spirally-curved configuration and preferentially adopts this configuration unless straightened by the presence of a stylet 60 or other straightening means.

20 In Figs. 7 and 8, the degree of curvature of the carrier member is illustrative only. The electrode array and carrier member may be formed and moulded, respectively, to adopt a greater or lesser degree of curvature than that depicted when the stylet 60 is fully retracted.

Each of the electrode sets and corresponding wires, are formed in a manner such that
25 their position with respect to each other is predetermined and kept constant throughout the process and in the final product.

While the electrode tip of the EDM equipment is depicted as having a particular arrangement depicted in Figs. 2A and 3A, it will be appreciated that the electrode tip can have other arrangements. The result of one such other arrangement is depicted in Fig. 4.
30 In this arrangement, use of the EDM tool results in the formation of five different electrodes sets, depicted as 41-45, respectively, on the one platinum sheet.

In Fig. 6, it can be seen that the stylet 60 passes through a lumen in the carrier member 61 formed by the folding of the electrodes 25 as defined above.

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The method described herein results in the formation of a carrier member for a cochlear implant system in which there has been no requirement to manually weld a wire to each electrode of the array. This serves to streamline the manufacturing process and allow greater automation thereof, resulting in suitable quality carrier members at a potentially lower cost. Further, the integrity of the platinum is maintained.

It will be appreciated by persons skilled in the art that numerous variations and/or modifications may be made to the invention as shown in the specific embodiments without departing from the spirit or scope of the invention as broadly described. For example, the techniques described could be applied to stimulating devices such as pacemakers, cochlear implants, FES stimulators; recording devices such as neural activity sensors and the like; implantable cables which may be used to connect implantable devices to other implantable devices or stimulating/sensing devices; and diagnostic devices capable of carrying out in-vivo analysis of body parameters.